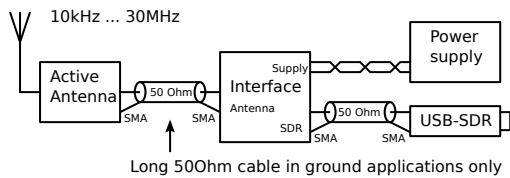
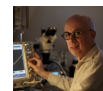


Design of a LF-HF Active Antenna in CMOS18 technology

Radio astronomy antenna for space applications

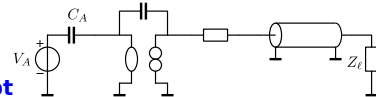


Antenna length: max 0.5m
 E-field antenna-referred noise:
 10kHz : 100n
 100kHz : 10n $\left[\frac{V}{\text{m}\sqrt{\text{Hz}}} \right]$
 1MHz : 5n
 30MHz : 5n
 Output 1dB compression level:
 0dBm in 500hm
 Antenna gain (-3dB: 10kHz-30MHz)
 0dB



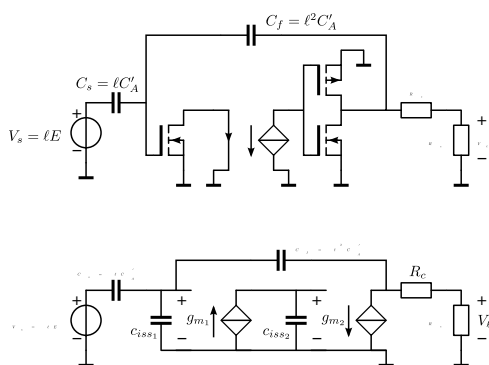
(c) 2021 Anton Montagne
 anton@montagne.nl
<https://www.analog-electronics.eu>

Features
 ESD discharge protected
 Low-power 1.8V CMOS technology



Amplifier concept

Design of a dual stage controller



$$L = -\frac{2g_{m1}g_{m2}R_c \frac{C_f}{C_f+C_s+c_{iss1}}}{s c_{iss2} \left(1 + s 2R_c \frac{C_f}{C_f+C_s+c_{iss1}} \right)}$$

$$LP_2 = \frac{g_{m1}g_{m2}}{c_{iss2}(C_s+c_{iss1})}$$

$$g_{m1} = 15.36\text{m}$$

$$g_{m2} = 23.62\text{m}$$

$$C_s = 5\text{p}$$

$$c_{iss1} = 7.568\text{p}$$

$$c_{iss2} = 0.4386\text{p}$$

$$B_f = \frac{1}{2\pi} \sqrt{LP_2} = 1.29\text{GHz}$$

$$p_1 = 0, p_2 = -\frac{C_f+C_s+c_{iss1}}{4\pi R_c C_f (C_s+c_{iss1})} = -763\text{MHz}$$

sum of poles (abs) increased as a result of pole-splitting
 in the second stage (first stage is shorted)

PZ analysis

PZ analysis results

Gain type: gain

DC gain = -1.000

pole	Re [Hz]	Im [Hz]	Mag [Hz]	Q
p1	-3.513e+8	-1.207e+9	1.257e+9	1.789
p2	-3.513e+8	1.207e+9	1.257e+9	1.789

zero	Re [Hz]	Im [Hz]	Mag [Hz]	Q
z1	2.176e+9	0	2.176e+9	0
z2	-3.978e+9	0	3.978e+9	0

PZ analysis results

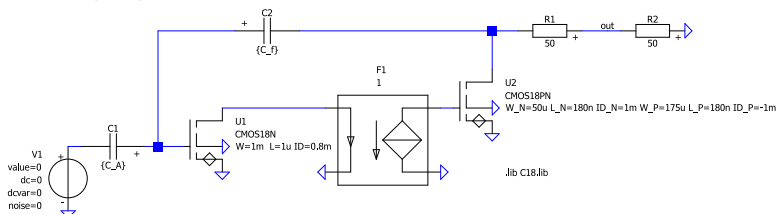
Gain type: loopgain

DC gain = oo

pole	Re [Hz]	Im [Hz]	Mag [Hz]	Q
p1	-1.038e+9	0	1.038e+9	0
p2	-1.038e+9	0	1.038e+9	0

zero	Re [Hz]	Im [Hz]	Mag [Hz]	Q
z1	5.315e+9	0	5.315e+9	0
z2	4.979e+10	0	4.979e+10	0

DualStage.py



Current mirror requirements

- Low noise:
 - Transconductance low compared to input stage
 - Low cut-off frequency (flicker noise)
- No dominant pole in loop gain
 - Current mirror introduces a pole at half the cut-off frequency
 - High cut-off frequency may conflict with low flicker noise

PZ analysis

PZ analysis results

Gain type: gain

DC gain = -0.9934

pole	Re [Hz]	Im [Hz]	Mag [Hz]	Q
p1	-3.829e+7	-5.721e+8	5.734e+8	7.488
p2	-3.829e+7	5.721e+8	5.734e+8	7.488
p3	-1.399e+9	0	1.399e+9	0

zero	Re [Hz]	Im [Hz]	Mag [Hz]	Q
z1	1.113e+9	0	1.113e+9	0
z2	-8.226e+8	-1.190e+9	1.447e+9	0.8793
z3	-8.226e+8	1.190e+9	1.447e+9	0.8793

PZ analysis results

Gain type: loopgain

DC gain = -151.5

pole	Re [Hz]	Im [Hz]	Mag [Hz]	Q	MFM bandwidth
p1	-6.324e+6	6.324e+6	6.324e+6	0	B1 = 963MHz
p2	-4.850e+8	4.850e+8	4.850e+8	0	B2 = 684MHz
p3	-9.838e+8	9.838e+8	9.838e+8	0	B3 = 772MHz

zero	Re [Hz]	Im [Hz]	Mag [Hz]	Q
z1	1.106e+10	0	1.106e+10	0
z2	4.979e+10	0	4.979e+10	0

Orthogonalize

- Separate the function (inverting unity-gain current amplifier) from its noise performance (low transconductance)
- Fix the transmittance with negative feedback

PZ analysis

PZ analysis results

Gain type: gain

DC gain = -0.9930

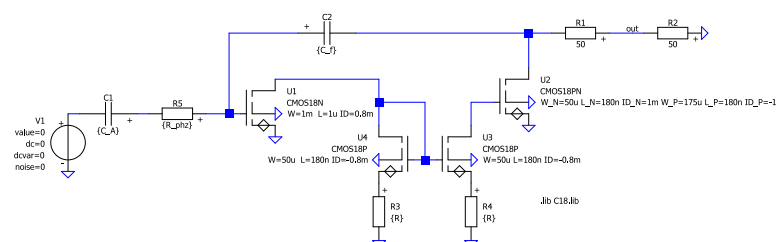
pole	Re [Hz]	Im [Hz]	Mag [Hz]	Q
p1	-7.126e+7	-9.490e+8	9.517e+8	6.677
p2	-7.126e+7	9.490e+8	9.517e+8	6.677
p3	-2.320e+9	0	2.320e+9	0
p4	-3.258e+10	0	3.258e+10	0

zero	Re [Hz]	Im [Hz]	Mag [Hz]	Q
z1	1.674e+9	0	1.674e+9	0
z2	-1.533e+9	-1.996e+9	2.516e+9	0.8209
z3	-1.533e+9	1.996e+9	2.516e+9	0.8209
z4	-3.261e+10	0	3.261e+10	0

Frequency compensation

- Second order system
- Influence of third pole cannot be ignored
- Compensation with phantom zero at the source introduces a fourth pole (resistor breaks loop of capacitors)
- Combination of pole-splitting and phantom-zero compensation

DualStageMirrorResComp1.py



DualStageMirrorResComp2.py

