

Design of noise performance of feedback amplifiers

The noisy nullor

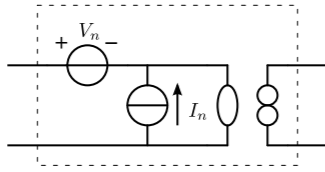
With a high-gain controller the source-load transfer is predominantly determined by the feedback network

We will show that this is not the case for the noise behavior

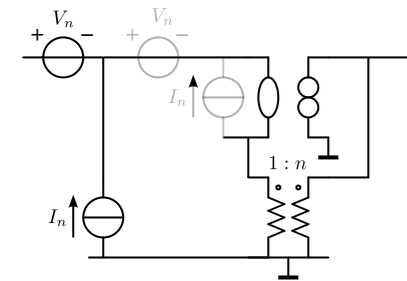
- Equivalent input noise sources of the controller should be kept small
- Deterioration of the signal to noise ratio by the feedback network should be kept small

Study the noise behavior of nonenergetic and passive feedback amplifiers

- Find rules for low-noise design
- Model the controller as a noisy nullor
- This enables orthogonal design of the noise behavior and of the static and dynamic transfer

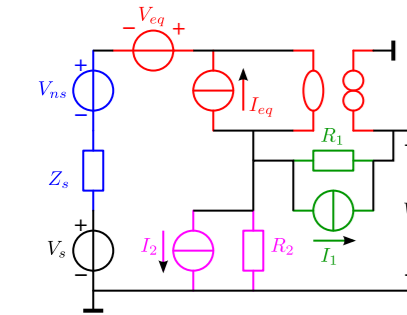


Noise performance of nonenergetic feedback amplifiers



Redirect the current noise source via ground
 Replace the equivalent input current noise source of the transformer with an equivalent output current noise source; use:
 $AD = 1, B = C = 0$
 The current source in parallel with the output of the nullor can be ignored. Replacing it with equivalent input sources yields zero because:
 $A = B = C = D = 0$

Noise performance of passive feedback amplifiers



Account for correlation:
 Use unique name for power spectral densities of uncorrelated sources.
 Add voltage or contributions of each uncorrelated source in one (complex) term.
 Multiply the power spectral density with the squared magnitude of this term

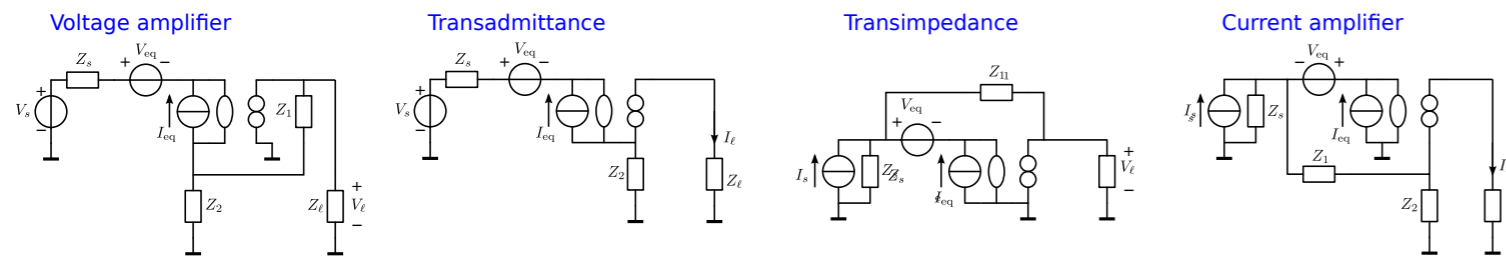
$$S_{V_{out}} = 4kTRe(Z_s) \left(\frac{R_1+R_2}{R_2}\right)^2 + S_{V_{eq}} \left(\frac{R_1+R_2}{R_2}\right)^2 + S_{I_{eq}} \left(\frac{R_1+R_2}{R_2}\right)^2 \left(Z_s + \frac{R_1 R_2}{R_1+R_2}\right)^2 + 4kT \frac{R_1^2}{R_2} + 4kT R_1$$

$$S_{V_s} = 4kTRe(Z_s) + S_{V_{eq}} + S_{I_{eq}} \left(Z_s + \frac{R_1 R_2}{R_1+R_2}\right)^2 \left(4kT \frac{R_1^2 R_2}{(R_1+R_2)^2} + 4kT \frac{R_1 R_2^2}{(R_1+R_2)^2}\right) \rightarrow +4kT \frac{R_1 R_2}{R_1+R_2}$$

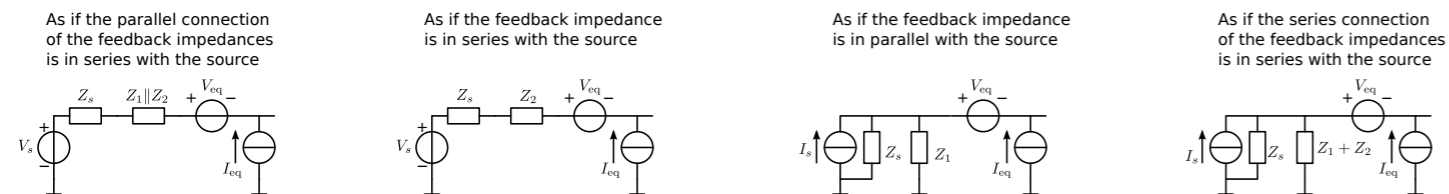
Conclusion:

The influence of the feedback resistors in the passive feedback voltage amplifier can be accounted for as if their parallel connection is in series with the source.

Single-loop passive feedback configurations and their equivalent input noise models



The noise contribution of the feedback impedances and their influence on the contribution of the equivalent input noise sources of the controller can be found:



SLiCAP noise analysis

```
#!/usr/bin/env python3
# -*- coding: utf-8 -*-
```

```
from SLiCAP import *

prj = initProject('Noisy Voltage Amplifier')

files = ['noisyVamp', 'noisyVampSimple']

noiseFigures = []

for fileName in files:
    makeNetlist(fileName + '.asc', fileName)
    il = instruction()
    il.setCircuit(fileName + '.cir')
    il.setSimType('symbolic')
    il.setGainType('vi')
    il.setData('noise')
    il.setDetector('V_out')
    il.setSource('V1')
    noiseResult = il.execute()

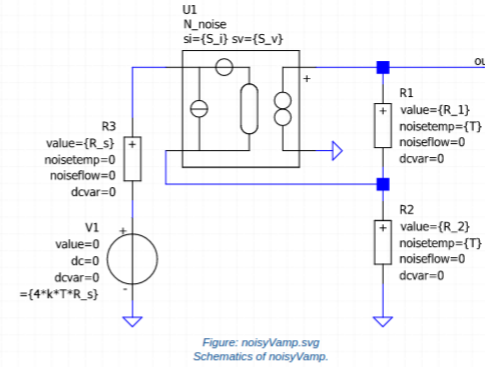
    htmlPage('Noise Analysis')
    head2html('Circuit diagram')
    img2html(fileName + '.svg', 600, label = 'fig_' +
        fileName, caption = 'Schematics of ' + fileName + '.')
    noise2html(noiseResult)

    # Print the noise figure
    F = noiseResult.inoise/noiseResult.inoiseTerms['V1']
    NF = 10*sp.log(F)/sp.log(10)
    noiseFigures.append(F)
```

```
ini.htmlIndex = 'index.html'
htmlPage('Noise figures')
head2html(files[0])
eqn2html('F', noiseFigures[0])
head2html(files[1])
eqn2html('F', noiseFigures[1])
head2html('Comparison')
Fdifference = sp.simplify(noiseFigures[0] - noiseFigures[1])
if sp.simplify(Fdifference) == 0:
    text2html('Both models have the same noise figure:')
else:
    text2html('Difference found between the noise figures obtained ' +
        'with the two models:')

eqn2html('F_' + files[0] + ' - F_' + files[1], Fdifference)
```

Circuit diagram



Symbolic noise analysis results

Detector-referred noise spectrum

$$S_{out} = \frac{4R_1^2 T k}{R_2} + 4R_1 T k + \frac{4R_1 T k (R_1 + R_2)^2}{R_2^2} + \frac{S_i (R_1 R_2 + R_1 R_s + R_2 R_s)^2}{R_2^2} + \frac{S_v (R_1 + R_2)^2}{R_2^2} \left[\frac{V^2}{Hz} \right]$$

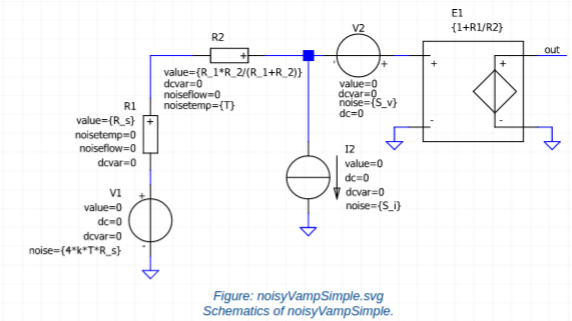
Source-referred noise spectrum

$$S_{in} = \frac{4R_1^2 R_2 T k}{(R_1 + R_2)^2} + \frac{4R_1 R_2^2 T k}{(R_1 + R_2)^2} + 4R_1 T k + \frac{S_i (R_1 R_2 + R_1 R_s + R_2 R_s)^2}{(R_1 + R_2)^2} + S_v \left[\frac{V^2}{Hz} \right]$$

Contributions of individual noise sources

Noise source: I1_XU1	$\left[\frac{A^2}{Hz} \right]$
Spectral density:	S_i
Detector-referred:	$\frac{S_i (R_1 R_2 + R_1 R_s + R_2 R_s)^2}{R_2^2}$
Source-referred:	$\frac{S_i (R_1 R_2 + R_1 R_s + R_2 R_s)^2}{(R_1 + R_2)^2}$
Noise source: I_noise_R1	$\left[\frac{A^2}{Hz} \right]$
Spectral density:	$\frac{4T k}{R_1}$
Detector-referred:	$4R_1 T k$
Source-referred:	$\frac{4R_1 R_2^2 T k}{(R_1 + R_2)^2}$
Noise source: I_noise_R2	$\left[\frac{A^2}{Hz} \right]$
Spectral density:	$\frac{4T k}{R_2}$
Detector-referred:	$\frac{4R_2^2 T k}{R_2}$
Source-referred:	$\frac{4R_1^2 R_2 T k}{(R_1 + R_2)^2}$
Noise source: V1	$\left[\frac{V^2}{Hz} \right]$
Spectral density:	$4R_s T k$
Detector-referred:	$\frac{4R_s T k (R_1 + R_2)^2}{R_2^2}$
Source-referred:	$4R_s T k$
Noise source: V1_XU1	$\left[\frac{V^2}{Hz} \right]$
Spectral density:	S_v
Detector-referred:	$\frac{S_v (R_1 + R_2)^2}{R_2^2}$
Source-referred:	S_v

Circuit diagram



Symbolic noise analysis results

Detector-referred noise spectrum

$$S_{out} = \frac{4R_1 R_2 T k (R_1 + R_2)^2}{R_2^2 (R_1 + R_2)} + \frac{4R_1 T k (R_1 + R_2)^2}{R_2^2} + \frac{S_i (R_1 + R_2)^2 (R_1 R_2 + R_1 R_s + R_2 R_s)^2}{R_2^2 (R_1 + R_2)^2} + \frac{S_v (R_1 + R_2)^2}{R_2^2} \left[\frac{V^2}{Hz} \right]$$

Source-referred noise spectrum

$$S_{in} = \frac{4R_1 R_2 T k}{R_1 + R_2} + 4R_1 T k + \frac{S_i (R_1 R_2 + R_1 R_s + R_2 R_s)^2}{(R_1 + R_2)^2} + S_v \left[\frac{V^2}{Hz} \right]$$

Contributions of individual noise sources

Noise source: I2	$\left[\frac{A^2}{Hz} \right]$
Spectral density:	S_i
Detector-referred:	$\frac{S_i (R_1 + R_2)^2 (R_1 R_2 + R_1 R_s + R_2 R_s)^2}{R_2^2 (R_1 + R_2)^2}$
Source-referred:	$\frac{S_i (R_1 R_2 + R_1 R_s + R_2 R_s)^2}{(R_1 + R_2)^2}$
Noise source: I_noise_R2	$\left[\frac{A^2}{Hz} \right]$
Spectral density:	$\frac{4T k (R_1 + R_2)}{R_1 R_2}$
Detector-referred:	$\frac{4R_1 R_2 T k (R_1 + R_2)^2}{R_2^2 (R_1 + R_2)}$
Source-referred:	$\frac{4R_1 R_2 T k}{R_1 + R_2}$
Noise source: V1	$\left[\frac{V^2}{Hz} \right]$
Spectral density:	$4R_s T k$
Detector-referred:	$\frac{4R_s T k (R_1 + R_2)^2}{R_2^2}$
Source-referred:	$4R_s T k$
Noise source: V2	$\left[\frac{V^2}{Hz} \right]$
Spectral density:	S_v
Detector-referred:	$\frac{S_v (R_1 + R_2)^2}{R_2^2}$
Source-referred:	S_v

Noise figures

noisyVamp

$$F = \frac{4R_1^2 R_2 T k \left(\frac{R_1}{R_2} + \frac{R_1}{R_s}\right) + 4R_1 R_2^2 T k + 4R_1 T k + \frac{S_i (R_1 R_2 + R_1 R_s + R_2 R_s)^2}{(R_1 + R_2)^2} + S_v}{4R_1 T k} \quad (1)$$

noisyVampSimple

$$F = \frac{4R_1^2 R_2 T k \left(\frac{R_1}{R_2} + \frac{R_1}{R_s}\right) + 4R_1 R_2^2 T k + \frac{S_i (R_1 R_2 + R_1 R_s + R_2 R_s)^2}{(R_1 + R_2)^2} + S_v}{4R_1 T k} \quad (2)$$

Comparison

Both models have the same noise figure:

$$F_{noisyVamp} - F_{noisyVampSimple} = 0 \quad (3)$$

Noisy Voltage Amplifier

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 SLiCAP: Symbolic Linear Circuit Analysis Program, Version 1.1 © 2009-2022 SLiCAP development team
 For documentation, examples, support, updates and courses please visit: analog-electronics.eu
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